# An Analog Electronics Companion

Basic Circuit Design for Engineers and Scientists

Scott Hamilton

Department of Physics and Astronomy University of Manchester



PUBLISHED BY THE PRESS SYNDICATE OF THE UNIVERSITY OF CAMBRIDGE The Pitt Building, Trumpington Street, Cambridge, United Kingdom

CAMBRIDGE UNIVERSITY PRESS The Edinburgh Building, Cambridge CB2 2RU, UK 40 West 20th Street, New York, NY 10011–4211, USA 477 Williamstown Road, Port Melbourne, VIC 3207, Australia Ruiz de Alarcón 13, 28014 Madrid, Spain Dock House, The Waterfront, Cape Town 8001, South Africa

http://www.cambridge.org

© Cambridge University Press 2003

This book is in copyright. Subject to statutory exception and to the provisions of relevant collective licensing agreements, no reproduction of any part may take place without the written permission of Cambridge University Press.

First published 2003

Printed in the United Kingdom at the University Press, Cambridge

Typeface Times NR MT 10.5/14 pt System QuarkXPress<sup>™</sup> [SE]

A catalogue record for this book is available from the British Library

Library of Congress Cataloguing in Publication data Hamilton, Scott, 1932– An analog electronics companion / Scott Hamilton. p. cm. Includes bibliographical references and index. ISBN 0 521 79838 8 1. Electronics. I. Title. TK7816.H35 2001 621.381–dc21 2001043081

ISBN 0 521 79838 8 hardback

### Contents

Preface	<i>page</i> xi
List of symbols and abbreviations	xvi

### Part 1 Mathematical techniques

1.1	Trigonometry	3
1.2	Geometry	6
1.3	Series expansions	9
1.4	Logarithms	12
1.5	Exponentials	16
1.6	Vectors	19
1.7	Complex numbers	28
1.8	Differentiation	34
1.9	Integration	37
1.10	Equations and determinants	42
1.11	Fourier transforms	49
1.12	Laplace transforms	60
1.13	Differential equations	76
1.14	Convolution	87

### Part 2 Physics

2.1	Current flow	93
2.2	Energies	97
2.3	Kirchhoff's laws	101
2.4	Faraday's law and Lenz's law	104
2.5	Currents and fields	107
2.6	Magnetism and relativity	113

2.7	Maxwell's equations	119
2.8	Conductivity and the skin effect	125
2.9	Quantization	131
2.10	Dielectrics and permittivity	135
2.11	Magnetic materials	139
2.12	Units of electromagnetism	147
2.13	Noise	150

### Part 3 Introduction to circuit mathematics

3.1	Circuit laws	159
3.2	A.C. theory	166
3.3	Phasors	173
3.4	Phase and amplitude	178
3.5	Resonance	183
3.6	Bandwidth and risetime	196
3.7	Pulse and transient response	206
3.8	Equivalent circuits	217
3.9	Cauchy's dog bodes well	225
3.10	Feedback	230
3.11	Noise in circuits	241
3.12	Hysteresis	252
3.13	Bridges	259
3.14	Approximation	263
3.15	Control systems	271
3.16	Filters	278
3.17	Transmission lines	293

### Part 4 Circuit elements

4.1	Resistors	307
4.2	Capacitors	312
4.3	Inductance	323
4.4	Transformers	331
4.5	Diodes	340
4.6	Bipolar transistors	349
4.7	Field effect transistors	357

1

4.8	Temperature dependent resistors	368
4.9	Coaxial cables	377
4.10	Crystals	383

### Part 5 SPICE circuit applications

5.1	Absolute value circuit	393
5.2	Oscilloscope probes	398
5.3	Operational amplifier circuits	403
5.4	Rectifier circuits	422
5.5	Integrators	431
5.6	Differentiator	436
5.7	Two-phase oscillator	444
5.8	Wien-bridge oscillator	449
5.9	Current sources and mirrors	458
5.10	Power supplies	464
5.11	Current-feedback amplifiers	479
5.12	Fast operational picoammeter	488
5.13	Three-pole, single amplifier filter	505
5.14	Open-loop response	511
5.15	Lumped or distributed?	523
5.16	Immittance Through the Looking Glass: gyrators, negative	
	immittance converters and frequency dependent negative resistors	527
5.17	Maser gain simulation	535
5.18	Frequency-independent phase shifter	539
5.19	Ratemeter	542
5.20	Baluns and high frequency transformers	545
5.21	Directional coupler	555
5.22	Power control or hotswitch	561
5.23	Modulation control of a resonant circuit	566
5.24	Photomultiplier gating circuit	571
5.25	Transatlantic telegraph cable	580
5.26	Chaos	588
5.27	Spice notes	598
Bibli	ography	615
Nam	ne index	621
Subj	ect index	629
Part	index	649

## 1.1 Trigonometry

The power of instruction is seldom of much efficacy except in those happy dispositions where it is almost superfluous.

Edward Gibbon

It may seem unexpected to find a section on trigonometry, but in electronics you cannot get away from sine waves. The standard definitions of sine, cosine and tangent in terms of the ratio of the sides of a right-angled triangle are shown in Fig. 1.1.1 and Eq. (1.1.1).

For angle  $\theta$  and referring to the sides of the triangle as opposite (*o*), adjacent (*a*) and hypotenuse (*h*) we have:

$$\sin \theta = \frac{o}{h}, \qquad \cos \theta = \frac{a}{h}, \qquad \tan \theta = \frac{o}{a}$$
 (1.1.1)

A common way to represent a sinusoidal wave is to rotate the phasor OA around the origin O at the appropriate rate  $\omega$  (in radians per second) and take the projection of OA as a function of time as shown in Fig. 1.1.2.

The corresponding projection along the x-axis will produce a cosine wave. This allows us to see the values of the functions at particular points, e.g. at  $\omega t = \pi/2$ ,  $\pi$ ,  $3\pi/2$  and  $2\pi$  as well as the signs in the four quadrants (Q). These are summarized in Table 1.1.1.



Fig. 1.1.1 Right-angled triangle.



Fig. 1.1.2 Projection of a rotating vector.

Table 1.1.1 Values and signs of trigonometrical functions in the four quadrants

Angle	0	$\pi/2$	$\pi$	$3\pi/2$	$2\pi$	1Q	2Q	3Q	4Q
Sin	0	1	0	1	0	+	+	_	_
Cos	1	0	1	0	1	+	_	_	+
Tan	0	$\infty$	0	$\infty$	0	+	_	+	-

Some useful relationships for various trigonometrical expressions are:

- (a)  $\sin(-\theta) = -\sin\theta$
- (b)  $\cos(-\theta) = \cos \theta$
- (c)  $\tan(-\theta) = -\tan\theta$
- (d)  $\cos(\theta + \phi) = \cos\theta \cdot \cos\phi \sin\theta \cdot \sin\phi$
- (e)  $\sin(\theta + \phi) = \sin\theta \cdot \cos\phi + \cos\theta \cdot \sin\phi$
- (f)  $\sin \theta + \sin \phi = 2\sin \frac{1}{2}(\theta + \phi) \cos \frac{1}{2}(\theta \phi)$
- (g)  $\cos \theta + \cos \phi = 2\cos \frac{1}{2}(\theta + \phi)\cos \frac{1}{2}(\theta \phi)$
- (h)  $\sin \theta \cdot \cos \phi = \frac{1}{2} [\sin (\theta + \phi) + \sin (\theta \phi)]$
- (i)  $\cos \theta \cdot \cos \phi = \frac{1}{2} [\cos (\theta + \phi) + \cos (\theta \phi)]$
- (j)  $\sin^2\theta + \cos^2\theta = 1$
- (k)  $\cos 2\theta = \cos^2 \theta \sin^2 \theta = 2\cos^2 \theta 1 = 1 2\sin^2 \theta$  (1.1.2)
- (1)  $1 + \cos \theta = 2\cos^2(\theta/2)$
- (m)  $1 \cos \theta = 2\sin^2(\theta/2)$
- (n)  $\sin 2\theta = 2\sin \theta \cos \theta$

(o) 
$$\lim_{\theta \to 0} \frac{\sin \theta}{\theta} = \lim_{\theta \to 0} \frac{\tan \theta}{\theta} = 1$$

- (p)  $\cos(\theta \phi) = \cos\theta \cdot \cos\phi + \sin\theta \cdot \sin\phi$
- (q)  $\sin(\theta \phi) = \sin \theta \cdot \cos \phi \cos \theta \cdot \sin \phi$
- (r)  $\sin \theta \sin \phi = 2\cos \frac{1}{2}(\theta + \phi) \sin \frac{1}{2}(\theta \phi)$
- (s)  $\cos \theta \cos \phi = 2\sin \frac{1}{2}(\phi + \theta) \sin \frac{1}{2}(\phi \theta)$
- (t)  $\cos \theta \cdot \sin \phi = \frac{1}{2} [\sin (\theta + \phi) \sin (\theta \phi)]$
- (u)  $\sin \theta \cdot \sin \phi = \frac{1}{2} [\cos (\theta \phi) \cos (\theta + \phi)]$

We will have occasion to refer to some of these in other sections and it should be remembered that the complex exponential expressions (Section 1.5) are often easier to use.

#### **References and additional sources 1.1**

- Fink D., Christansen D. (1989): *Electronics Engineer's Handbook*, 3<sup>rd</sup> Edn, New York: McGraw-Hill. ISBN 0-07-020982-0
- Korn G. A., Korn T. M. (1989): Mathematics, formula, definitions, and theorems used in electronics engineering. In Fink D., Christansen D. *Electronics Engineer's Handbook*, 3<sup>rd</sup> Edn, Section 2, New York: McGraw-Hill.
- Lambourne R., Tinker M. (Eds) (2000): *Basic Mathematics for the Physical Sciences*, New York: John Wiley. ISBN 0-471-85207-4.

Langford-Smith F. (1954): Radio Designer's Handbook, London: Illife and Sons.

Terman F.E. (1950): Radio Engineers' Handbook, New York: McGraw-Hill.

## 1.2 Geometry

For geometry by itself is a rather heavy and clumsy machine. Remember its history, and how it went forward with great bounds when algebra came to its assistance. Later on, the assistant became the master.

Oliver Heaviside (1899): Electromagnetic Theory, April 10, Vol. II, p. 124

The relationship between equations and their geometric representation is outlined in Section 1.10. In various places we will need to make use of Cartesian (coordinate) geometry either to draw graphical responses or to determine various parameters from the graphs.

A commonly used representation of the first order, or single pole, response of an operational amplifier in terms of the zero frequency (z.f.) gain  $A_0$  and the corner frequency  $\omega_c = 1/T$  is given by:

$$A = \frac{A_0}{1+sT} \tag{1.2.1}$$

which on the log-log scales usually used is as shown in Fig. 1.2.1.



Fig. 1.2.1 Operational amplifier response.

At low frequency  $sT \ll 1$  so the gain is just  $A_0$ . At high frequency  $sT \gg 1$  so the gain is  $A_0/sT$  as shown. The graphs are slightly different from those with standard x- and y-axes, which are of course where y=0 and x=0, because here we have logarithmic scales. The traditional x- and y-axes would then be at  $-\infty$ , which is not useful. We can start by taking G=1 and f=1 for which the log values are zero (log 1=0). You can of course draw your axes at any value you wish, but decade intervals are preferable. The slope of  $A_0/sT$  can be determined as follows. Take two frequencies  $\omega_a$  and  $\omega_b$  as shown. The slope, which is the tangent of the angle  $\theta$ , will be given (allowing for the sense of the slope) by:

$$\tan \theta = \frac{\log\left(\frac{A_0}{\omega_a T}\right) - \log\left(\frac{A_0}{\omega_b T}\right)}{\log(\omega_b) - \log(\omega_a)}$$

$$= \frac{\log\left(\frac{\omega_b}{\omega_a}\right)}{\log\left(\frac{\omega_b}{\omega_a}\right)}$$

$$= 1 \quad \text{and} \quad \theta = \tan^{-1}(1) = 45^{\circ}$$
(1.2.2)

where we have used the fact that the difference of two logs is the log of the quotient (Section 1.4). Since the slope does not depend on  $\omega$  then  $A_0/sT$  must be a straight line on the log-log scales.

A point of interest on the amplifier response is the unity-gain (or transition) frequency  $\omega_T$  as this defines the region of useful performance and is particularly relevant to considerations of stability. We need to find the value of  $\omega$  for which G=1. Note that though we use the more general complex frequency s we can simply substitute  $\omega$  for s since we are dealing with simple sine waves and are not concerned with phase since this is a graph of amplitude. Thus we have:

$$1 = \frac{A_0}{\omega_T T} \quad \text{or} \quad \omega_T = \frac{A_0}{T} \tag{1.2.3}$$

and remember that  $\omega$  is an angular frequency in rad s<sup>-1</sup> and  $f = \omega / 2\pi$  Hz. Say we now wish to draw the response for a differentiator which has  $G = sR_fC_i$ (Section 5.6). The gain will be 1 when  $\omega_D = 1/R_fC_i$  and the slope will be 45°. So fixing point  $\omega_D$  and drawing a line at 45° will give the frequency response. To find where this line meets the open-loop response we have:

$$sR_fC_i = \frac{A_0}{sT}$$
 or  $s^2 = \frac{A_0}{R_fC_iT}$  so  $\omega_P = \left(\frac{A_0}{R_fC_iT}\right)^{\frac{1}{2}}$  (1.2.4)

which is shown in Fig. 1.2.2.



Fig. 1.2.2 Geometry of differentiator frequency response.

#### **References and additional sources 1.2**

- Hambley A. R. (1994): *Electronics. A Top-Down Approach to Computer-Aided Circuit Design*, New York: Macmillan. ISBN 0-02-349335-6. See Appendix B.
- Lambourne R., Tinker M. (Eds) (2000): *Basic Mathematics for the Physical Sciences*, New York: John Wiley. ISBN 0-471-85207-4.
- Tobey G. E., Graeme J. G., Huelsman L. P. (1971): *Operational Amplifiers. Design and Applications*, New York: McGraw-Hill. Library of Congress Cat. No. 74-163297.
- Van Valkenburg M. E. (1982): Analog Filter Design, New York: Holt, Rinehart and Winston. ISBN 0-03-059246-1, or 4-8338-0091-3 International Edn. See Chapter 3.

## **1.3** Series expansions

Prof. Klein distinguishes three main classes of mathematicians – the intuitionists, the formalists or algorithmists, and the logicians. Now it is intuition that is most useful in physical mathematics, for that means taking a broad view of a question, apart from the narrowness of special mathematics. For what a physicist wants is a good view of the physics itself in its mathematical relations, and it is quite a secondary matter to have logical demonstrations. The mutual consistency of results is more satisfying, and exceptional peculiarities are ignored. It is more useful than exact mathematics.

But when intuition breaks down, something more rudimentary must take its place. This is groping, and it is experimental work, with of course some induction and deduction going along with it. Now, having started on a physical foundation in the treatment of irrational operators, which was successful, in seeking for explanation of some results, I got beyond the physics altogether, and was left without any guidance save that of untrustworthy intuition in the region of pure quantity. But success may come by the study of failures. So I made a detailed study and close examination of some of the obscurities before alluded to, beginning with numerical groping. The result was to clear up most of the obscurities, correct the errors involved, and by their revision to obtain correct formulae and extend results considerably.

Oliver Heaviside (1899): Electromagnetic Theory, April 10, Vol. II, p. 460

Expansion of functions in terms of infinite (usually) series is often a convenient means of obtaining an approximation that is good enough for our purposes. In some cases it also allows us to obtain a relationship between apparently unconnected functions, and one in particular has been of immense importance in our and many other fields. We will list here some of the more useful expansions without derivation (Boas 1966):

$$\sin \theta = \theta - \frac{\theta^3}{3!} + \frac{\theta^5}{5!} - \frac{\theta^7}{7!} + \cdots$$

$$\cos \theta = 1 - \frac{\theta^2}{2!} + \frac{\theta^4}{4!} - \frac{\theta^6}{6!} + \cdots$$

$$e^x = 1 + x + \frac{x^2}{2!} + \frac{x^3}{3!} + \frac{x^4}{4!} + \cdots$$
(1.3.1)

where

$$n! \equiv n(n-1)(n-2)(n-3) \cdots 1$$

and *n*! is known as *n* factorial. Note that, odd though it may seem, 0! = 1. The variable  $\theta$  must be in radians.

The binomial series is given by:

$$(1+x)^{n} = 1 + nx + \frac{n(n-1)x^{2}}{2!} + \frac{n(n-1)(n-2)x^{3}}{3!} + \cdots$$
(1.3.2)

valid for *n* positive or negative and |x| < 1

which is most frequently used for  $x \ll 1$  to give a convenient approximation:

$$(1+x)^n \cong 1+nx$$
 (1.3.3)

The geometric series in x has a sum  $S_n$  to n terms given by:

$$a + ax^{2} + ax^{3} + ax^{4} + \dots + ax^{n} + \dots +, \text{ with sum } S_{n} = \frac{a(1 - x^{n})}{1 - x}$$
 (1.3.4)

and for |x| < 1 the sum for an infinite number of terms is:

$$S = \frac{a}{1 - x} \tag{1.3.5}$$

In some circumstances, when we wish to find the value of some function as the variable goes to a limit, e.g. zero or infinity, we find that we land up with an indeterminate value such as 0/0,  $\infty/\infty$  or  $0 \times \infty$ . In such circumstances, if there is a proper limit, it may be determined by examining how the function approaches the limit rather than what it appears to do if we just substitute the limiting value of the variable. As an example consider the function (Boas 1966, p. 27):

$$\lim_{x \to 0} \frac{1 - e^x}{x}, \text{ which becomes } \frac{0}{0} \text{ for } x = 0$$
(1.3.6)

If we expand the exponential using Eq. (1.3.1), then remembering that x is going to become very small:

$$\lim_{x \to 0} \frac{1 - e^x}{x} = \lim_{x \to 0} \frac{1 - \left(1 + x + \frac{x^2}{2!} + \cdots\right)}{x} = \lim_{x \to 0} \left(-1 - \frac{x}{2!} - \cdots\right) = -1$$
(1.3.7)

Expansion in terms of a series, as in this case, is generally most useful for cases where  $x \rightarrow 0$ , since in the limit the series is reduced to the constant term. There is another approach, known as l'Hôpital's rule (or l'Hospital), which makes use of a Taylor series expansion in terms of derivatives. If the derivative of f(x) is f'(x), then:

$$\lim_{x \to 0} \frac{f(x)}{\phi(x)} = \lim_{x \to 0} \frac{f'(x)}{\phi'(x)}$$
(1.3.8)

but the ease of use depends on the complexity of the differentials. The Taylor series referred to allows expansion of a function f(x) around a point x = a:

$$f(x) = f(a) + (x - a)f'(a) + \frac{(x - a)^2}{2!}f''(a) + \dots + \frac{(x - a)^n}{n!}f^n(a)$$
(1.3.9)

where f(a), f'(a), etc. is the value of the quantity for x = a. If the expansion is around the origin, x = 0, the series is sometimes referred to as Maclaurin's series.

#### **References and additional sources 1.3**

- Boas M. L. (1966): *Mathematical Methods in the Physical Sciences*, New York: John Wiley. Library of Congress Cat. No. 66-17646.
- Courant R. (1937): *Differential and Integral Calculus*, 2<sup>nd</sup> Edn, Vols 1 and 2. London: Blackie and Son.
- James G., Burley D., Clements D., Dyke P., Searl J., Wright J. (1996): *Modern Engineering Mathematics*, 2<sup>nd</sup> Edn, Wokingham: Addison-Wesley. ISBN 0-201-87761-9.
- Pipes L. A. (1958): *Applied Mathematics for Engineers and Physicists*, New York: McGraw-Hill. Library of Congress Cat. No. 57-9434.
- Poularikas A. D. (Ed.) (1996): The Transforms and Applications Handbook, Boca Raton: CRC Press and IEEE Press. ISBN 0-8493-8342-0.

## 1.4 Logarithms

God created the whole numbers: all the rest is man's work.

Leopold Kronecker (1823-1891)

Logarithms, originally developed to help in complex calculations, are now largely superseded for hand calculation by the ubiquitous calculator or mathematical software on your PC. However, we still need to know about them in a number of circumstances and most particularly in electronics they help us cope with numbers spanning a wide range. In a Bode plot of gain, for example, a linear scale will show only a small portion of the range with any resolution and low gains will be inaccessible. Log scales are very common therefore and the decibel 'unit' is used in many areas from aircraft noise to attenuation in optical fibres.

We list now some of the basic relations for logarithms (Abramowitz and Stegun 1970). Logarithms relate to a base value, say  $\beta$ , in the following way. For generality we will write **lgm** for reference to an arbitrary base. If:

$$y = \beta^x$$
 then  $\lg m_{\beta}(y) = x$  (1.4.1)

and on this basis we can write:

$$\lg m(ab) = \lg m(a) + \lg m(b) \qquad \lg m\left(\frac{a}{b}\right) = \lg m(a) - \lg m(b)$$
$$\lg m(a^n) = n \lg m(a) \qquad \qquad \lg m\left(\frac{a^n}{b}\right) = \frac{1}{n} \lg m(a) \qquad (1.4.2)$$

 $\lg_{\beta}(a) = \frac{\lg_{\alpha}(a)}{\lg_{\alpha}(\beta)}$ , for conversion between bases  $\beta$  and  $\alpha$ 

 $\lg m(1) = 0 \qquad \qquad \lg m(0) = -\infty$ 

The two common bases are  $\beta = 10$ , for which is written log, and  $\beta = e = 2.71828$ ..., which is written ln and which are called natural logarithms. We can then list the additional relations for ln:



Fig. 1.4.1 Graph of the logarithmic functions.

$$\ln(1+x) = x - \frac{x^2}{2} + \frac{x^3}{3} - \frac{x^4}{4} + \cdots$$
  

$$\ln(n+1) = \ln(n) + 2\left[\frac{1}{(2n+1)} + \frac{1}{3}\frac{1}{(2n+1)^3} + \frac{1}{5}\frac{1}{(2n+1)^5} + \cdots\right] \quad \text{for } n > 0 \quad (1.4.3)$$
  

$$\frac{d}{dx}[\ln(x)] = \frac{1}{x} \qquad \int \frac{dx}{x} = \ln(x)$$

The value of  $\ln(0) = -\infty$  is the reason *PROBE* in PSpice will refuse to display on a log scale if the data include zero. The use of logarithmic scales is discussed below. The form of the logarithm is shown in Fig. 1.4.1.

It might appear that there are no logarithms for negative numbers, but this is only true if we are restricted to real numbers (Section 1.7). For complex numbers negative arguments are allowed though we will not make use of this possibility. In fact a number, positive or negative will now have an infinite set of logarithms. For example (n is an integer):

$$\ln(-1) = \ln(re^{j\theta}) = \ln(r) + \ln(e^{j\theta}) = \ln(1) + j(\pi + 2n\pi) = j\pi, -j\pi, 3j\pi, \dots$$
(1.4.4)

As mentioned above the very wide range of many of the quantities met in electronics, together with the convenience of simple addition, rather than multiplication, for sequential gains when expressed in a logarithmic scale, prompted the widespread adoption of logarithmic measures. Early measures of attenuation were made in terms of a length of standard cable (Everitt and Anner 1956). To obtain a more generally usable and convenient measure a unit was chosen that closely matched the older version and later it was named the decibel in honour of Alexander Graham Bell. Though the actual unit is the bel, closer agreement with the earlier measures was achieved at one-tenth of this, i.e. the decibel and this has over time become the most commonly used unit. The proper definition is given as a power ratio and could represent both attenuation or gain. If the two powers are  $P_1$  and  $P_2$  then:

Power gain or ratio 
$$G_p = 10 \log\left(\frac{P_1}{P_2}\right) dB$$
 (1.4.5)

If  $P_1$  is greater than  $P_2$  then we have gain expressed as +dB whereas if the powers are in the opposite sense then we have attenuation expressed as -dB. If the resistances R at which the powers are measured are the same, then since  $P = V^2/R$  we may also write:

$$G_p = 10 \log\left(\frac{V_1^2}{V_2^2}\right) = 20 \log\left(\frac{V_1}{V_2}\right) dB$$
 (1.4.6)

The convenience of logarithmic scales has led to widespread use, sometimes bending the rules, which has caused argument in the literature (Simons 1973; Page 1973), but the improper usages have by now become so established that political correctness has been discarded. When we talk of voltage gains using Eq.(1.4.6) to determine the dB value, the usual difference of impedance levels is ignored. So long as we are all agreed and understand the usage there should be no confusion, but it is as well to be aware of the approximation. It should always be made clear whether power or voltage (or current) is being referred to as the measure will be different. Many derivative units have subsequently been defined such as dBm which refers to a power gain where the reference level (e.g.  $P_2$  above) is 1 mW, so that 0 dBm = 1 mW.

An associated reason for using logarithmic scales is that (some of) our senses, e.g. hearing or vision, are logarithmic in sensitivity. This was expressed in the Weber–Fechner law, which holds that 'the minimum change in stimulus necessary to produce a perceptible change in response is proportional to the stimulus already existing' (Everitt and Anner 1956, p. 244). Such responses are illustrated by the audibility sensitivity curves averaged over many subjects in the early 1930s (e.g. Terman 1951); one wonders if measurements at the present time on subjects exposed to the extreme volumes of modern 'music' would reveal the same results.

#### **References and additional sources 1.4**

- Abramowitz M., Stegun I. A. (1970): *Handbook of Mathematical Functions with Formulas, Graphs and Mathematical Tables*, Applied Mathematics Series, Washington: National Bureau of Standards.
- Everitt W. L., Anner G. E. (1956): *Communication Engineering*, 3<sup>rd</sup> Edn, New York: McGraw-Hill. Library of Congress Cat. No. 55-12099. See pp. 241–247.
- Lambourne R., Tinker M. (Eds) (2000): *Basic Mathematics for the Physical Sciences*, New York: John Wiley. ISBN 0-471-85207-4.

Page C. (1973): Logarithmic quantities and units. Proc. IEEE 61, 1516–1518.

- Pipes L. A. (1958): *Applied Mathematics for Engineers and Physicists*, 2<sup>nd</sup> International Student Edn, New York: McGraw-Hill. Library of Congress Cat. No. 57-9434. See p. 29.
- Simons K. (1973): The dB anything. Proc. IEEE 61, 495–496.

Terman F. E. (1951): Radio Engineering, 3rd Edn, London: McGraw-Hill. See p. 864.

## **1.5** Exponentials

There must be an ideal world, a sort of mathematician's paradise where everything happens as it does in textbooks.

Bertrand Russell

The exponential function occurs frequently in electronics. It represents phenomena where the rate of change of a variable is proportional to the value of the variable. In a more abstract form we will meet it in Section 1.7 where we will find a most useful relation between it and the trigonometrical functions. Let us consider a more practical circumstance, the charging of a capacitor (Fig. 1.5.1).

We assume that the capacitor is uncharged (this is not essential) and at time t=0 the switch is closed. At this instant  $V_C$  is zero so the current  $i = V_{in}/R = i_0$ . We require to find the variation of  $V_C$  with time. At any time when the current is *i* and the charge on *C* is *Q*,  $V_C$  will be given by:

$$V_{C} = \frac{Q}{C} \quad \text{so that} \quad dV_{C} = \frac{dQ}{C} = \frac{i \, dt}{C}, \quad \text{where} \quad i = \frac{V_{in} - V_{C}}{R}$$

$$\text{so } \frac{dV_{C}}{dt} = \frac{i}{C} = \frac{V_{in} - V_{C}}{RC}$$
(1.5.1)



Fig. 1.5.1 Current flow in a capacitor.

This fits with the statement above about the exponential function except that the rate of change  $dV_c/dt$  is proportional to  $V_{in} - V_C$ , so that as  $V_C$  increases towards its final value  $V_{in}$  the rate of change will decrease. There is a formal method of solving this differential equation for  $V_C$  but we will take the easier path by guessing (knowing) the answer and showing that it agrees with Eq. (1.5.1). We try:

$$V_C = V_{in}(1 - e^{-t/RC}) \tag{1.5.2}$$

To see if this is in agreement with (1.5.1) we differentiate to give:

$$\frac{dV_C}{dt} = 0 + \frac{V_{in}}{RC} e^{-t/RC}$$

$$= \frac{V_{in}}{RC} \left(\frac{V_{in} - V_C}{V_{in}}\right) = \frac{V_{in} - V_C}{RC}$$
(1.5.3)

where we have substituted for  $e^{-t/RC}$  from Eq. 1.5.2, and see that (1.5.2) is a solution of Eq. (1.5.1). We also have:

$$i = \frac{V_{in} - V_C}{R} = \frac{V_{in}}{R} e^{-t/RC} = i_0 e^{-t/RC}, \quad \text{where} \quad i_0 = \frac{V_{in}}{R}$$
(1.5.4)

The initial slope of  $V_C$  is given by the value of  $dV_C/dt$  at t=0. From Eq. (1.5.3):

$$\left(\frac{dV_C}{dt}\right)_{t=0} = \frac{V_{in}}{RC}$$
(1.5.5)

The quantity  $RC = \tau$  is called the time constant. The initial slope tangent will reach  $V_{in}$  at time  $\tau$ . The exponent -t/RC must be dimensionless so that the units of RC must be time. This can be checked:

$$C = \frac{Q}{V} = \frac{\text{Coulomb}}{\text{Volt}} = \frac{\text{Amp sec}}{\text{Volt}} \quad \text{and} \quad R = \frac{\text{Volt}}{\text{Amp}}$$
so 
$$RC = \frac{\text{Volt}}{\text{Amp}} \frac{\text{Amp sec}}{\text{Volt}} = \sec$$
(1.5.6)

It is often a useful check when doing some complex algebra to examine the consistency of the units of all the terms to see if they are compatible. Any inconsistency can alert you to errors in your algebra. Units are discussed in Section 2.12.

The voltage  $V_R$  across R is just the difference between  $V_{in}$  and  $V_C$ . Thus we have from Eq. (1.5.2):

$$V_R = V_{in} - V_C = V_{in} e^{-t/RC}$$
(1.5.7)

The form of the various functions are shown in Fig. 1.5.2.

Theoretically  $V_C$ , for example, never reaches  $V_{in}$ . The time to reach within a given percentage of  $V_{in}$  can be calculated and must be allowed for when making more



Fig. 1.5.2 Exponential responses and initial slopes.

Table 1.5.1 Approach of an exponential function to the final value

Time $ au$	0	1	2	3	4	5	6	7
$V_C/V_{in}$	0	0.632	0.865	0.950	0.982	0.993	0.998	0.999
$V_R/V_{in}$	1	0.368	0.135	0.050	0.018	0.007	0.002	0.001

accurate measurements. Table 1.5.1 shows the difference as a function of multiples of the time constant  $\tau$ . For example at time  $t = \tau = RC$  the value of  $V_C$  is  $\approx 63\%$  of  $V_{in}$  and you must wait for seven time constants to be within 0.1% of  $V_{in}$ .

If we consider a similar circuit to Fig. 1.5.1 with an inductor replacing the capacitor then a similar analysis leads to the result:

$$i_L = i_0 (1 - e^{-tR/L}), \quad \text{with} \quad i_0 = V_{in}/R$$
 (1.5.8)

and in this case the time constant is  $\tau = L/R$ .

#### **References and additional sources 1.5**

- Courant R. (1937): *Differential and Integral Calculus*, 2<sup>nd</sup> Edn, Vols 1 and 2, London: Blackie and Son. See Chapter III, Section 6.
- Lambourne R., Tinker M. (Eds) (2000): *Basic Mathematics for the Physical Sciences*, New York: John Wiley. ISBN 0-471-85207-4.
- Walton A. K. (1987): Network Analysis and Practice, Cambridge: Cambridge University Press. ISBN 0-521-31903-X. See Appendix 2.

## **1.6** Vectors

Also, he should remember that unfamiliarity with notation and processes may give an appearance of difficulty that is entirely fictitious, even to an intrinsically easy matter; so that it is necessary to thoroughly master the notation and ideas involved. The best plan is to sit down and work; all that books can do is to show the way.

Oliver Heaviside (1891): Electromagnetic Theory, Nov. 13, Vol. I, p. 139

In discussing electromagnetic topics it is necessary to make use of vectors since many of the quantities involved have both magnitude and direction. The algebra of vectors is a little messy but if we can understand the vector relationships things become much neater and easier to write. There are a number of very useful theorems which allow us to transform relations to suit our purposes: we will state and describe how they work. Vectors are written in bold italic type, e.g. *A*.

The addition and subtraction of vectors follows the simple parallelogram geometry as discussed in Section 1.7 and the possible circumstance of three dimensions simply requires two successive operations. Subtraction also follows the same technique. Vectors may be resolved along any suitable set of coordinates, such as Cartesian or polar, but for our purposes we can restrict our choice to Cartesian.

Multiplication presents us with two different possibilities. Any vector A, say, may be resolved into components along a chosen set of rectangular coordinates x, y and z, with components  $A_x$ ,  $A_y$  and  $A_z$  (Fig. 1.6.1).

The magnitude of the vector is then given by:

Magnitude = 
$$(A_x^2 + A_y^2 + A_z^2)^{\frac{1}{2}}$$
 (1.6.1)

We can define the *scalar product*, shown by  $A \cdot A$  (sometimes also called the dot product) by:

$$A \bullet A = A_x^2 + A_y^2 + A_z^2 \tag{1.6.2}$$

which is a scalar, i.e. it has no direction, only magnitude. It is just the square of the length of the vector A and, though the components will change,  $A \cdot A$  is independent of the axes chosen. The scalar product of two different vectors A and B is defined in a similar way as:

$$\boldsymbol{A} \boldsymbol{\bullet} \boldsymbol{B} = \boldsymbol{A}_{x} \boldsymbol{B}_{x} + \boldsymbol{A}_{y} \boldsymbol{B}_{y} + \boldsymbol{A}_{z} \boldsymbol{B}_{z} \tag{1.6.3}$$

20



Fig. 1.6.1 Vector components.

and an alternative form can be expressed in terms of the lengths, A and B, of the two vectors and the angle  $\theta$  between them (Fig. 1.6.2):

$$\boldsymbol{A} \boldsymbol{\bullet} \boldsymbol{B} = \boldsymbol{A} \boldsymbol{B} \boldsymbol{\cos} \, \boldsymbol{\theta} \tag{1.6.4}$$

and it is evident that the order of the vectors is immaterial, i.e.  $A \cdot B = B \cdot A$ .

It is often convenient to make use of *unit vectors* along each of the three axes x, y and z. These are usually represented by the vector symbols i, j and k, respectively (it is perhaps unfortunate that i is also used in complex numbers, and that we use j instead in electronics, but the context should make the meaning clear; there are just not enough symbols to go round for everything to have its own). The scalar products of these vectors can be readily deduced from Eq. (1.6.4) to give:

$$i \cdot i = 1 \qquad j \cdot j = 1 \qquad k \cdot k = 1$$
  

$$i \cdot j = 0 \qquad j \cdot k = 0 \qquad k \cdot i = 0$$
(1.6.5)

and we can use the unit vectors to express any vector in the form:

$$A = iA_{x} + jA_{y} + kA_{z} \tag{1.6.6}$$

Some quantities multiply in a quite different way. You may be aware that the force acting on a charge moving in a magnetic field is proportional to the product of velocity and field but acts in a direction normal to both velocity and field. This



Fig. 1.6.2 Vector scalar or dot product.



Fig. 1.6.3 Vector cross product.

requires the definition of another form of multiplication known as the *vector or* cross product shown by  $A \times B$  which is itself a vector (some books use the symbol  $\land$  instead of  $\times$ ). The magnitude is most directly defined by:

$$\boldsymbol{A} \times \boldsymbol{B} = \boldsymbol{A}\boldsymbol{B}\sin\theta \tag{1.6.7}$$

and the direction of the vector is normal to the plane containing A and B and in the sense of the advancement of a right-handed screw rotated from A to B, and shown as C in Fig. 1.6.3. It is evident that reversing the order of A and B gives the same magnitude but the opposite direction, i.e.  $B \times A = -C$ .

The consequences for unit vectors are:

$$i \times i = j \times j = k \times k = 0$$
  

$$i \times j = k, \quad j \times k = i, \quad k \times i = j$$
(1.6.8)

If we write the vectors in the form of Eq. (1.6.6) and carry out the multiplications using (1.6.8), then we have:

$$A \times B = (iA_x + jA_y + kA_z) \times (iB_x + jB_y + kB_z)$$
  
=  $i(A_yB_z - A_zB_y) + j(A_zB_x - A_xB_z) + k(A_xB_y - A_yB_x)$   
=  $\begin{vmatrix} i & j & k \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$  (1.6.9)

where the last line expresses the relation in the form of a determinant (Section 1.10) and is much easier to recall.

We will be making use of vector algebra for dealing with electromagnetic field quantities, which vary both with respect to position and with time. We therefore need to examine how we can differentiate and integrate vectors. Taking a vector in the form of Eq. (1.6.6), then if say the vector is a function of *t* we have:

$$\frac{dA}{dt} = i\frac{dA_x}{dt} + j\frac{dA_y}{dt} + k\frac{dA_z}{dt}$$
(1.6.10)

which is a vector whose components are the derivatives of the components of A. If we have a field representing a simple scalar quantity  $\phi(x, y, z)$ , (temperature is a good example), then we can ask what is the steepest slope or gradient at any point and this will evidently depend on the slope in the direction of each of the axes. The result is found to be the gradient of  $\phi$ :

grad 
$$\phi = i \frac{\partial \phi}{\partial x} + j \frac{\partial \phi}{\partial y} + k \frac{\partial \phi}{\partial z}$$
 (1.6.11)

and is evidently also a vector. The use of  $\partial$  signifies that when differentiating only quantities depending on what you are differentiating with respect to are relevant, e.g. in the first term those depending on x are relevant while those depending on y or z are considered constants. The form found here arises frequently and it is convenient to define a symbol to represent this in the form of an operator, for example just like say d/dt:

$$\nabla = i\frac{\partial}{\partial x} + j\frac{\partial}{\partial y} + k\frac{\partial}{\partial z} \qquad (1.6.12)$$

The vector operator  $\nabla$  is called *del* and only has meaning when operating on something. Thus we have that  $\nabla \phi \equiv \text{grad } \phi$  as in Eq. (1.6.11).  $\nabla$  can also operate on a vector. If we have a field described by a vector function V(x, y, z) where the components  $V_x$ ,  $V_y$  and  $V_z$  of V are functions of x, y and z:

$$V(x, y, z) = iV_{x}(x, y, z) + jV_{y}(x, y, z) + kV_{z}(x, y, z)$$
(1.6.13)

then we can define the *divergence* of V by:

div 
$$V \equiv \nabla \cdot V = \frac{\partial V_x}{\partial x} + \frac{\partial V_y}{\partial y} + \frac{\partial V_z}{\partial z}$$
 (1.6.14)

which is a scalar. We can also define the *curl* of V by:

$$\operatorname{curl} \boldsymbol{V} \equiv \boldsymbol{\nabla} \times \boldsymbol{V} = \boldsymbol{i} \left( \frac{\partial V_z}{\partial y} - \frac{\partial V_y}{\partial z} \right) + \boldsymbol{j} \left( \frac{\partial V_x}{\partial z} - \frac{\partial V_z}{\partial x} \right) + \boldsymbol{k} \left( \frac{\partial V_y}{\partial x} - \frac{\partial V_x}{\partial y} \right)$$
(1.6.15)

and this is a vector. Since the gradient is a vector function we can define a further useful relation by taking the divergence of it:

div grad 
$$\phi \equiv \nabla \cdot \nabla \phi = \frac{\partial}{\partial x} \frac{\partial \phi}{\partial x} + \frac{\partial}{\partial y} \frac{\partial \phi}{\partial y} + \frac{\partial}{\partial z} \frac{\partial \phi}{\partial z}$$
  
$$= \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} + \frac{\partial^2 \phi}{\partial z^2} \equiv \nabla^2 \phi$$
(1.6.16)

and this is a very important expression. The operator  $\nabla^2$  is called the Laplacian and is a scalar operator. For example an equation of the form:

$$\nabla^2 \phi = \frac{1}{a^2} \frac{\partial^2 \phi}{\partial t^2} \tag{1.6.17}$$

is a wave equation as we will come across in examining the consequences of Maxwell's equations. If we reverse the order of div and grad and apply this to a vector, then:

### grad div $V \equiv \nabla (\nabla \cdot V)$ $=\boldsymbol{i}\left(\frac{\partial^2 V_x}{\partial x^2} + \frac{\partial^2 V_y}{\partial x \partial y} + \frac{\partial^2 V_z}{\partial x \partial z}\right) + \boldsymbol{j}\left(\frac{\partial^2 V_x}{\partial x \partial y} + \frac{\partial V_y}{\partial y^2} + \frac{\partial^2 V_z}{\partial y \partial z}\right) + \boldsymbol{k}\left(\frac{\partial^2 V_x}{\partial x \partial z} + \frac{\partial^2 V_y}{\partial y \partial z} + \frac{\partial^2 V_z}{\partial z^2}\right) (1.6.18)$

and now it becomes more evident that the symbolic forms can save a lot of writing. Since  $\nabla^2$  is a scalar, the operation on a vector is simply a vector with components:

$$\nabla^2 V \equiv \nabla \cdot \nabla V = (\nabla^2 V_x, \nabla^2 V_y, \nabla^2 V_z)$$
(1.6.19)

One further relation will be needed which is defined by:

$$\nabla \times (\nabla \times V) = \nabla (\nabla \cdot V) - (\nabla \cdot \nabla) V$$
  
=  $\nabla (\nabla \cdot V) - \nabla^2 V$   
r curl curl  $V$  = grad div  $V$  - del<sup>2</sup>  $V$  (1.6.20)

curl curl V = grad div V - del<sup>2</sup> Vor

The divergence of a cross product will be required in Section 2.2:

$$\nabla \bullet (A \times B) = B \bullet (\nabla \times A) - A \bullet (\nabla \times B)$$
(1.6.21)